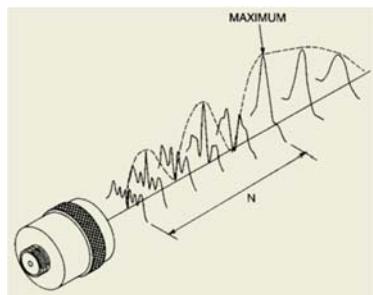
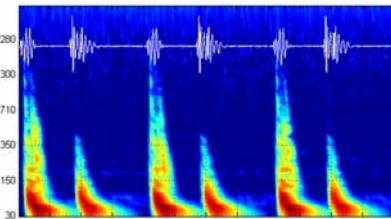


Physics of ultrasonography

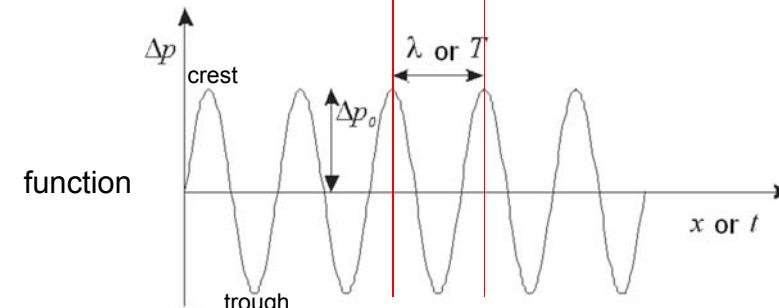
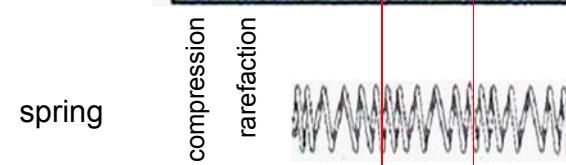


KAD 2015.03.24



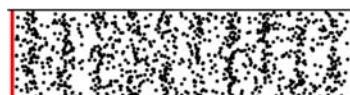
2

Sound: mechanical wave (model)



spatial and temporal periodicity

2



longitudinal wave
(in the interior of liquids and gases only this type)



transverse wave

hydrostatic pressure

pressure change,
sound pressure

$$p_{\text{total}} = p_{\text{hydrostat}} + \Delta p$$

pressure DC + AC

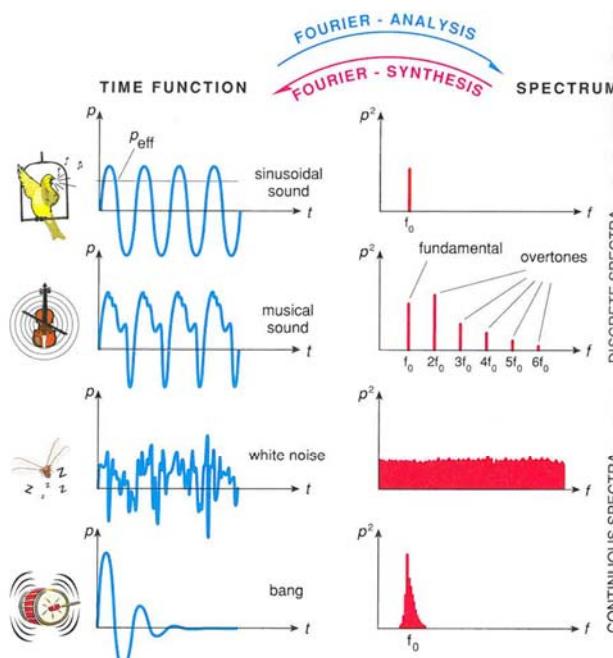
amplitude

$$\Delta p(t, x) = \Delta p_{\max} \sin\left[2\pi\left(\frac{t}{T} - \frac{x}{\lambda}\right)\right]$$

$$c \cdot T = \lambda, \quad c = f \cdot \lambda$$

Textbook, Fig. II.46.

3



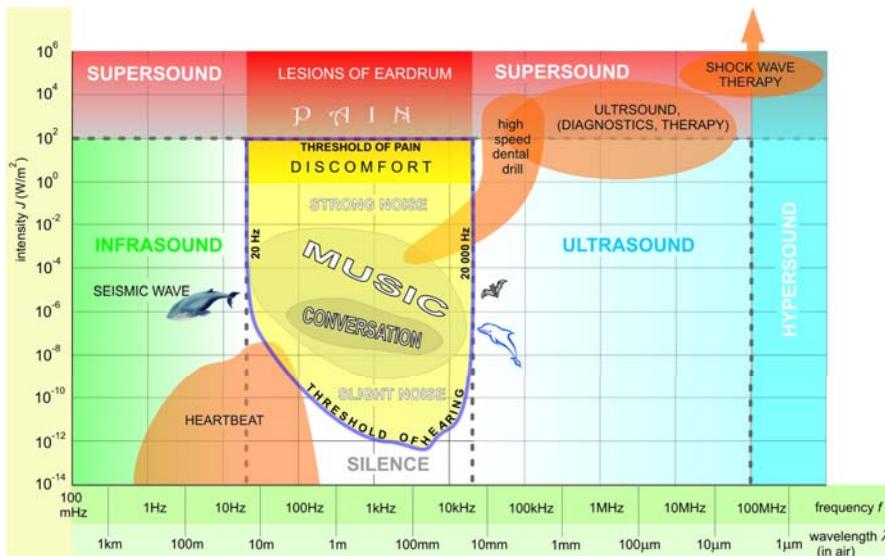
pitch:
frequency of the fundamental

timbre (tone colour):
relative strengths of overtones/harmonics (spectrum)

4

Textbook, Fig. IV.23.

Frequency and intensity regions of sounds



Lab. manual, Audiometry.

5



The role of elastic medium

$$\kappa = -\frac{\Delta V}{V} \frac{1}{\Delta p}$$

compressibility
relative volume decrease
over pressure

$$c = \frac{1}{\sqrt{\rho \kappa}}$$

speed of sound

$$Z = \frac{p}{v} = \frac{p_{\max}}{v_{\max}}$$

acoustic impedance
(definition)

$$Z_{el} = \frac{U}{I}$$

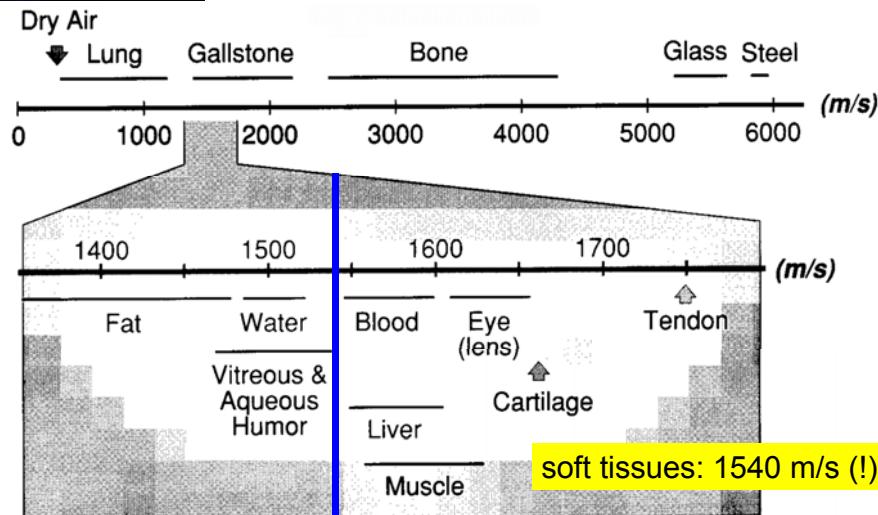
$$Z = c\rho = \sqrt{\frac{\rho}{\kappa}}$$

acoustic impedance
(useful form)

6



Speed of sound/US in different media



7

Intensity of US

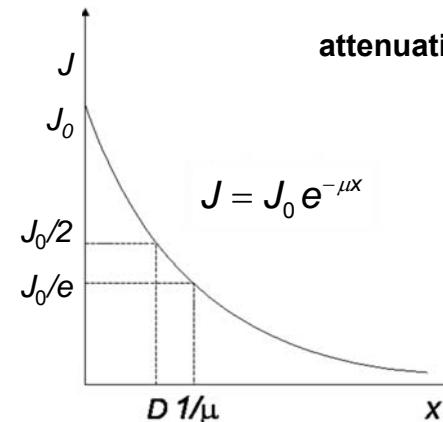
$$J = \frac{1}{Z} \Delta p_{eff}^2$$

intensity =
energy-current density

$$P_{el} = \frac{1}{Z_{el}} U_{eff}^2$$

electric analogy

Loss of energy during propagation (absorption)



$$\text{attenuation: } \alpha = 10 \cdot \lg \frac{J_0}{J} \text{ dB}$$

$$\alpha = 10 \cdot \mu \cdot x \cdot \lg e \text{ dB}$$

μ is proportional to
frequency in the
diagnostic range

$$\text{specific attenuation: } \frac{\alpha}{f \cdot x}$$

8

μ is proportional to frequency in the diagnostic range

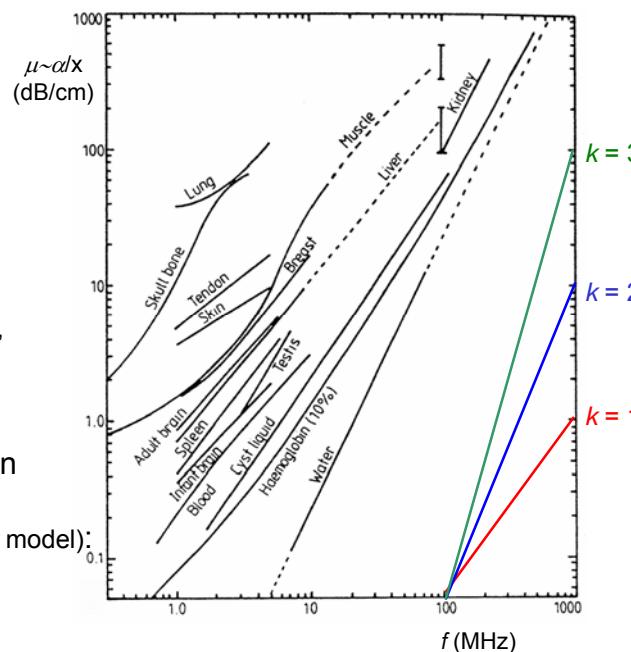
$$\mu \sim f^k, \quad k \sim 1 (?)$$

$$\log \mu \sim k \log f$$

if the graph is a linear, the power function approximation is valid

specific attenuation for soft tissues
(homogeneous tissue model):

$$\frac{\alpha}{f x} \sim 1 \text{ dB cm MHz}$$



9

Reflection (normal incidence)

reflectivity:

$$R = \frac{J_{\text{reflected}}}{J_{\text{incident}}} = \left(\frac{Z_1 - Z_2}{Z_1 + Z_2} \right)^2$$

"full" reflection:

$$Z_1 \ll Z_2, \quad R \approx 1$$

optimal coupling:

$$Z_{\text{connecting}} \approx \sqrt{Z_{\text{source}} Z_{\text{skin}}}$$

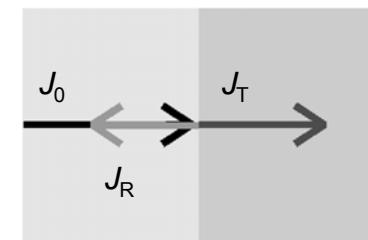


boundary surface	R
muscle/blood	0.001
fat/liver	0.006
fat/muscle	0.01
bone/muscle	0.41
bone/fat	0.48
soft tissue/air	0.99

11

Phenomena at the boundary of different media

normal/perpendicular incidence

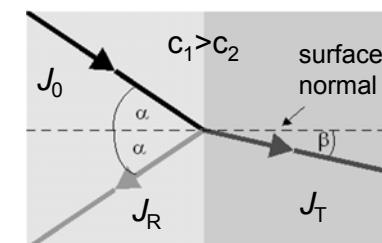


$$J_0 = J_R + J_T$$

reflection and transmission
(penetration)

Textbook, Fig. II.47.

skew incidence

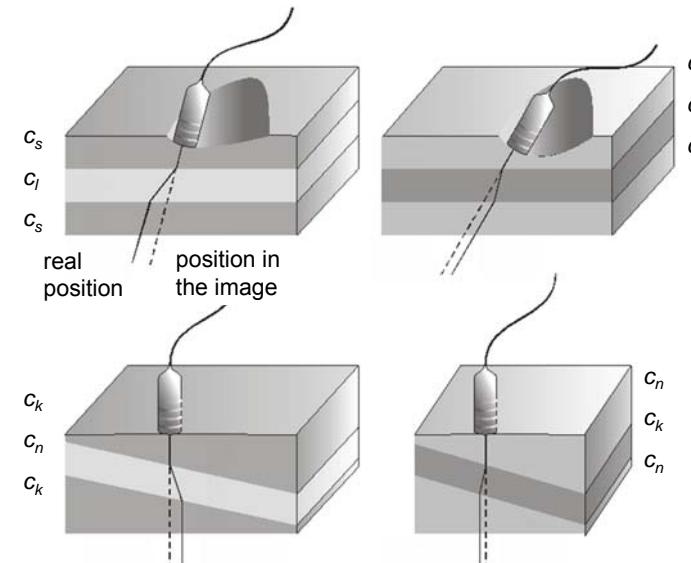


$$\frac{\sin \alpha}{\sin \beta} = \frac{c_1}{c_2}$$

Snellius-Descartes

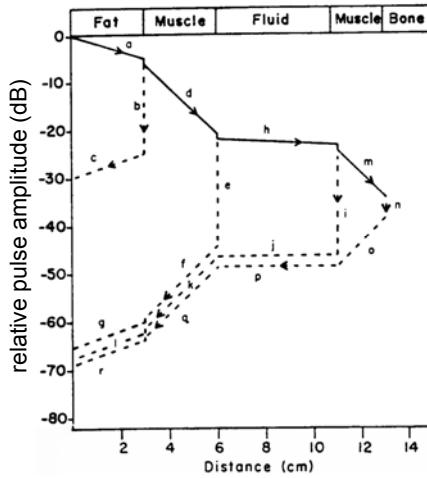
10

Phenomenon of skew incidence or normal incidence and skew boundaries



Textbook, Fig. on pg. 153

12



Absorption and reflection

the later comes back the reflection, the deeper lays the reflecting surface and the weaker is the intensity
run time dependent amplification

TGC: time gain compensation

DGC: depth gain control

boundary surface	R	$10\lg R$ (dB)	T	$10\lg T$ (dB)
fat/muscle	0.01	-20.0	0.990	-0.044
muscle/blood	0.001	-30.0	0.999	-0.004
muscle/bone	0.41	-3.9	0.590	-2.291

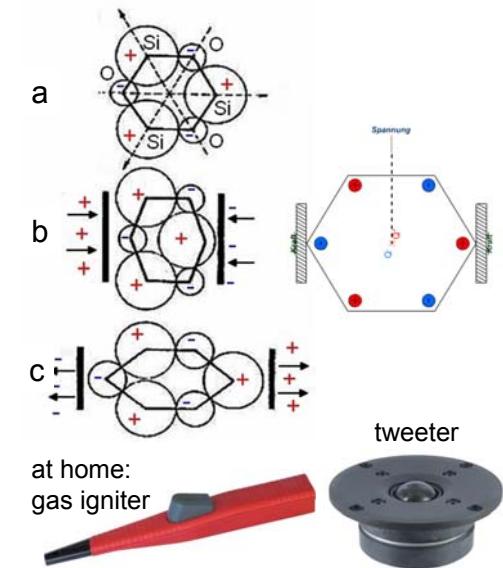
13

Generation of US. Piezoelectric effect

source of electric signal
(sine wave oscillator)+
transducer (piezo-crystal)

(a) Center of charge of positive and negative charges coincides.

(b) and (c) As a result of pressure, the charge centers are separated, i.e. a potential difference arises (direct ~).
The crystal is deformed when voltage is applied (inverse ~).

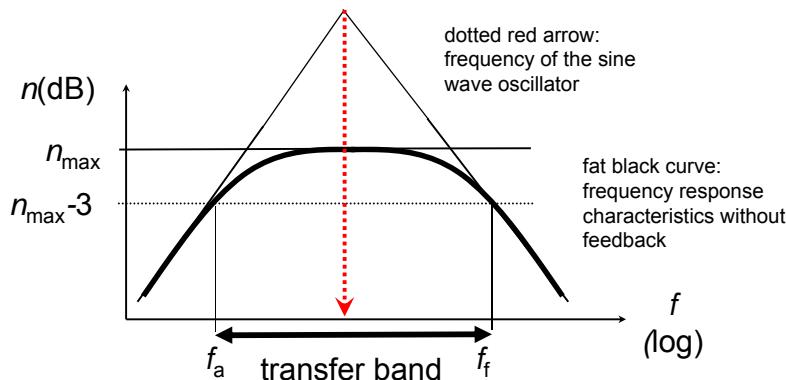


Source of electric signal : sine wave oscillator

amplifier with positive feedback

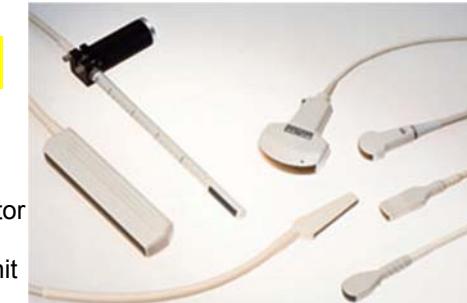
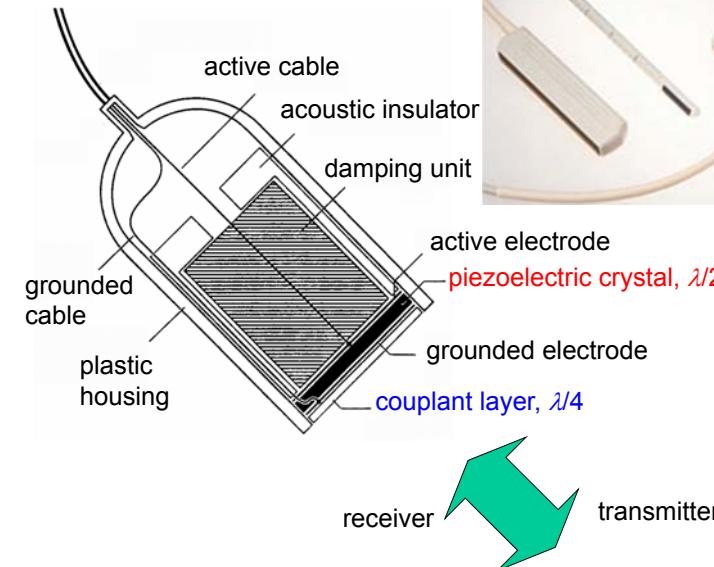
$$A_{U, \text{feedback}} = \frac{A_U}{1 - \beta A_U}$$

$\beta A_U = 1$, amplification = "infinity" → sine wave oscillator
no input signal, output signal: sine voltage



15

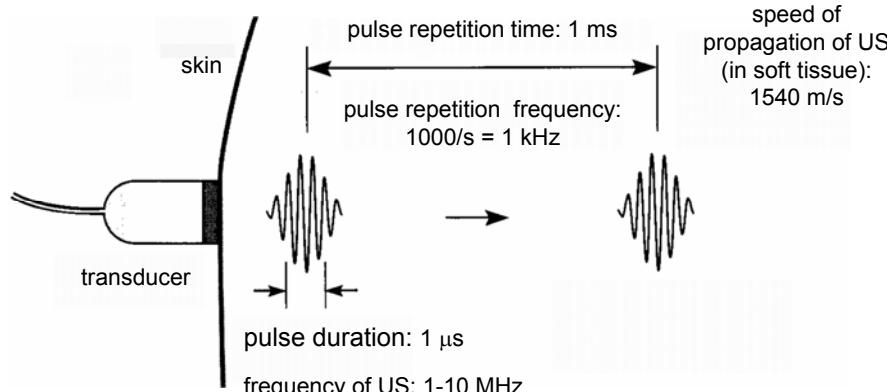
Ultrasound transducer



16

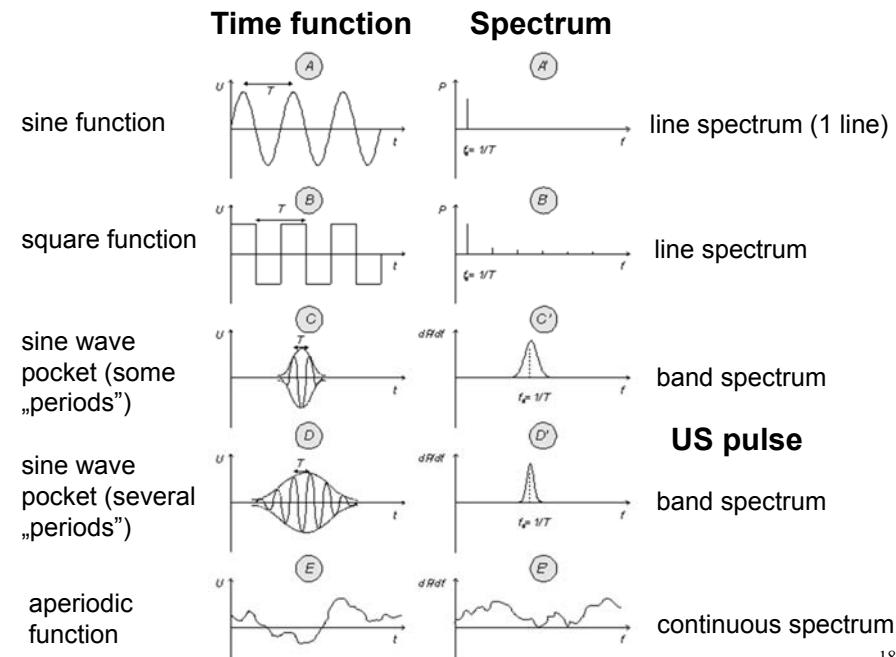
Characteristic of US pulses

transducer: transmitter and receiver is the same unit
time sharing mode: pulses instead of continuous wave



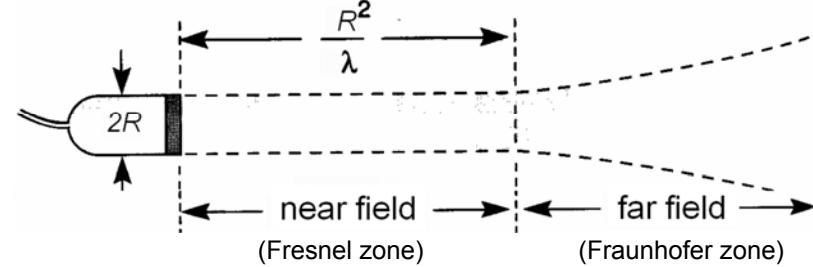
Textbook, Fig. VIII.32.

17

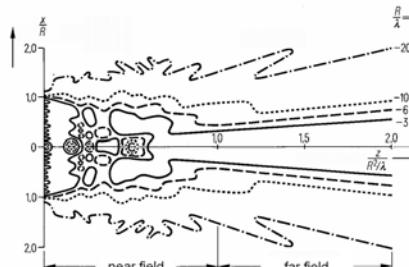


18

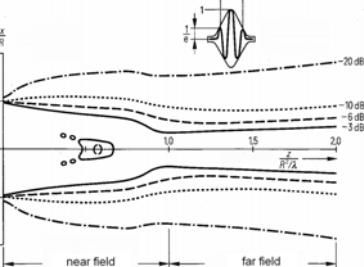
US beam shape (simplified version)



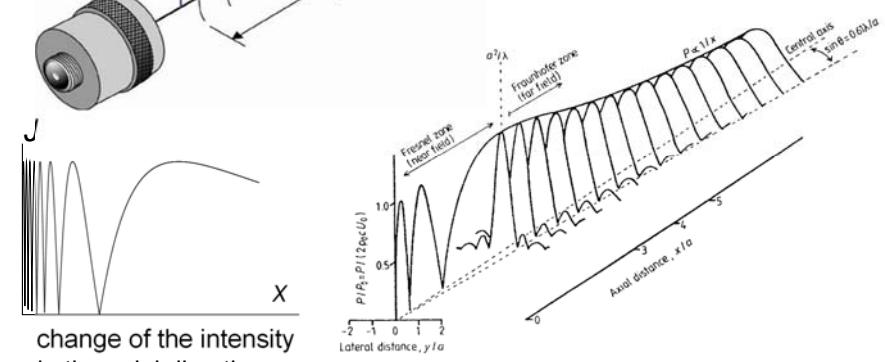
Beam shape, continuous wave US



Beam shape, pulsed wave US



Perspective view of the US beam



change of the intensity
in the axial direction

cf. Textbook. Fig. on p.505

20

Resolving limit, resolution

Resolving limit is the distance between two object details which can be just resolved as distinct objects (the smaller the better).

Resolution (resolving power): the reciprocal of the resolving limit (the greater the better)

Axial resolving limit depends on the pulse length. Pulse length is inversely proportional to the frequency.

Typical values	frequency (MHz):	2	15
	wavelength (in muscle) (mm):	0.78	0.1
	penetration depth (cm):	12	1.6
	lateral resolving limit (mm):	3.0	0.4
	axial resolving limit (mm):	0.8	0.15

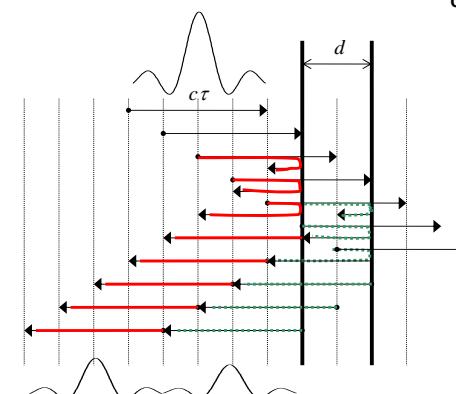
21

Axial resolving limit

τ : pulse duration

$c_1\tau \approx c_2\tau = c\tau$ pulse length

$$\delta_{ax} = d = \frac{c\tau}{2} \text{ resolving limit}$$

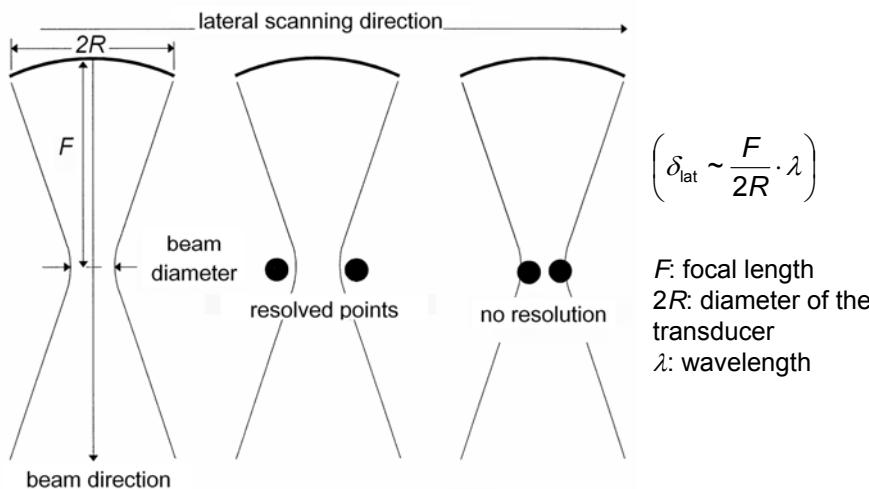


The axial resolving limit is the half of the pulse length. The echos from the adjacent surfaces in this case just hit another.

$$\tau \sim T = \frac{1}{f}$$

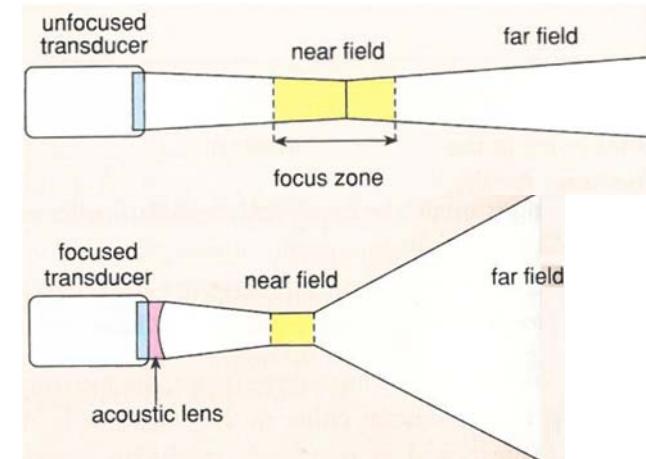
22

Lateral resolving limit



23

Focusing of the beam

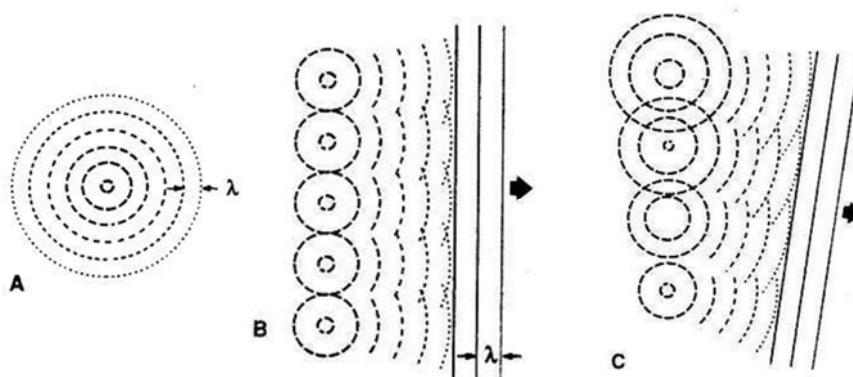


Focusing increases the divergence of the beam in the far field regime and reduces the depth sharpness.

cf. Textbook Fig. on p.506

24

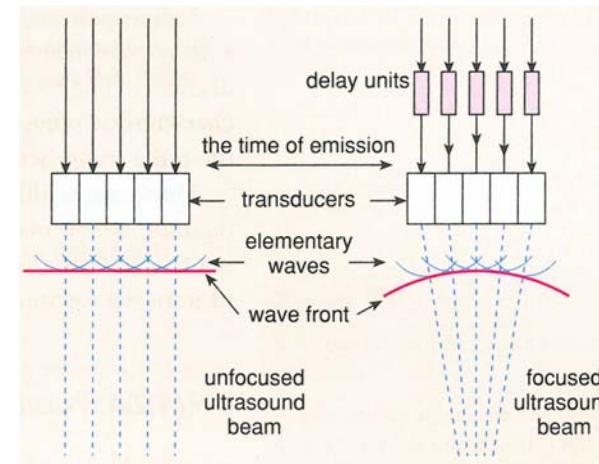
Huygens' principle



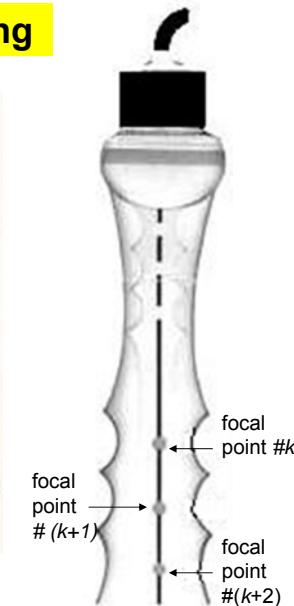
Any wave propagates so, that each point on a primary wavefront serves as the source of spherical secondary wavelets that advance with a speed and frequency equal to those of the primary wave. The primary wavefront at some later time is the envelope of these wavelets.

25

Electronic focusing



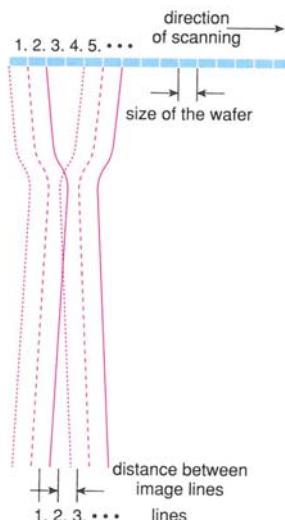
cf. Textbook Fig. on p.507



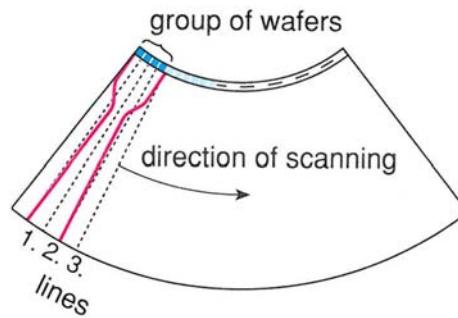
26

Scanning

multi unit linear array

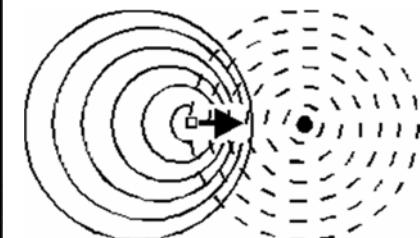
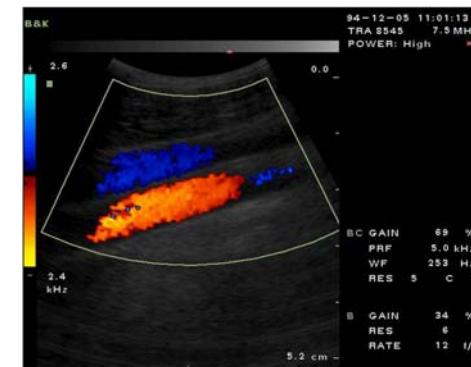


multi unit curved array



27

US imaging. Modes of sonography. Doppler-echo.

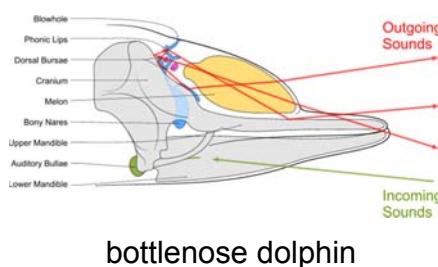
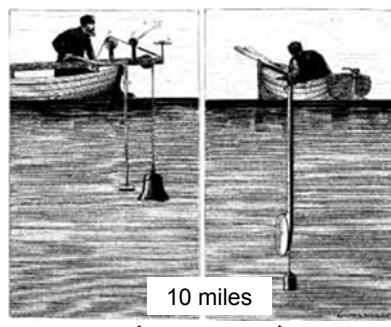


cf. Textbook Fig. VII. 36-37

Echo principle

1794 Spallanzani:
bat's navigation

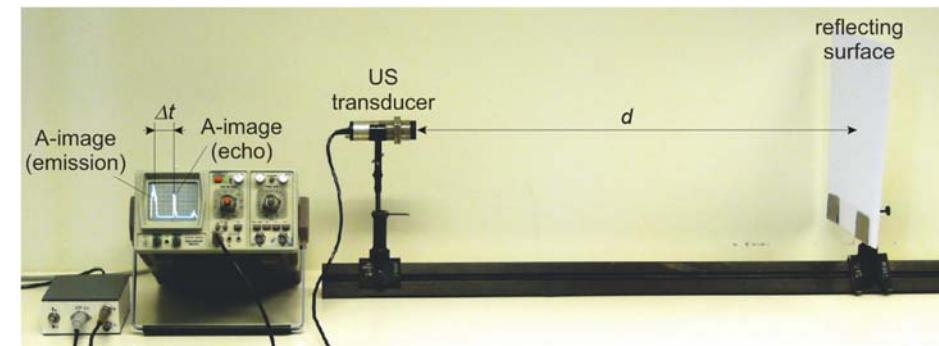
1822 Colladen
measured the speed of
sound in water



29

Echo principle

using a special US-head, short pulses are emitted in the air towards a reflecting surface, and the same US-head detects the echo signal

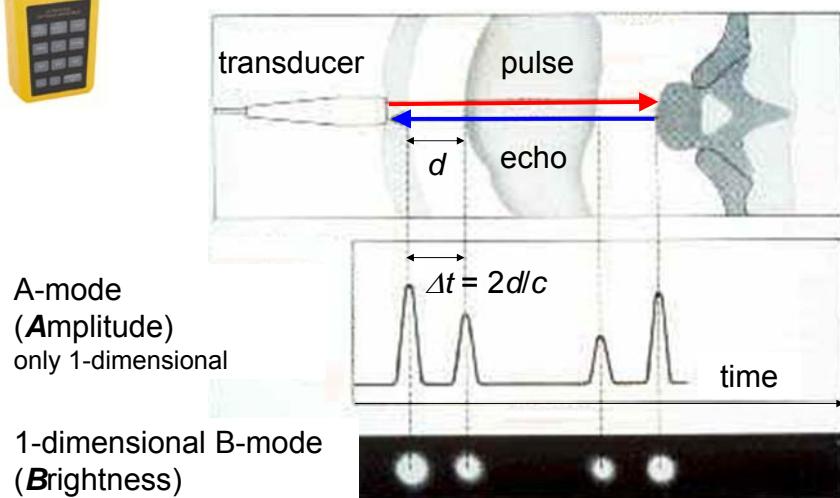


$$c\Delta t = d+d = 2d$$

30

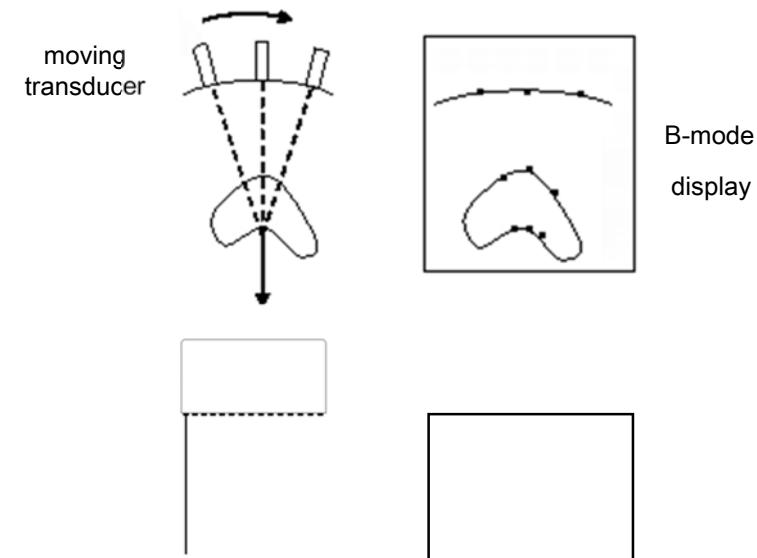


Receiving the echos



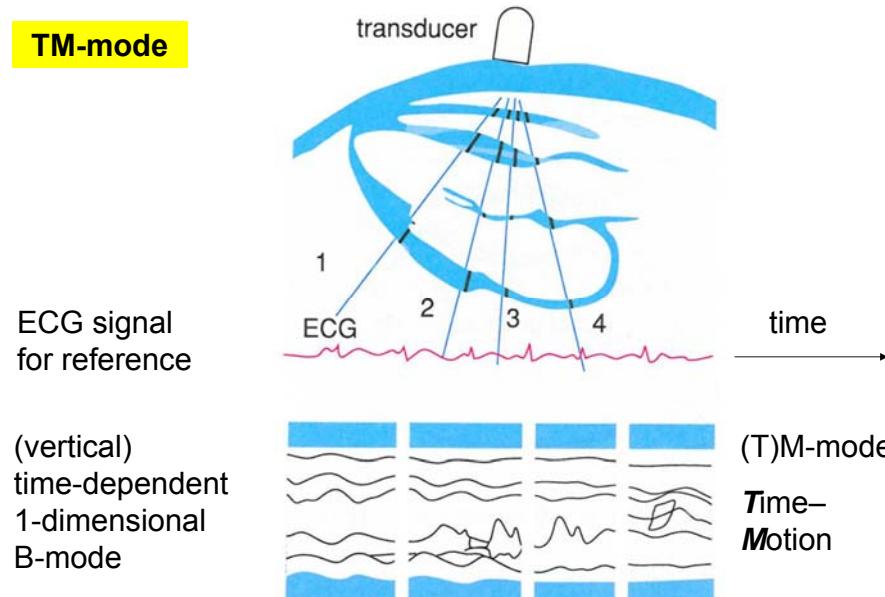
31

2-dimensional B-mode



32

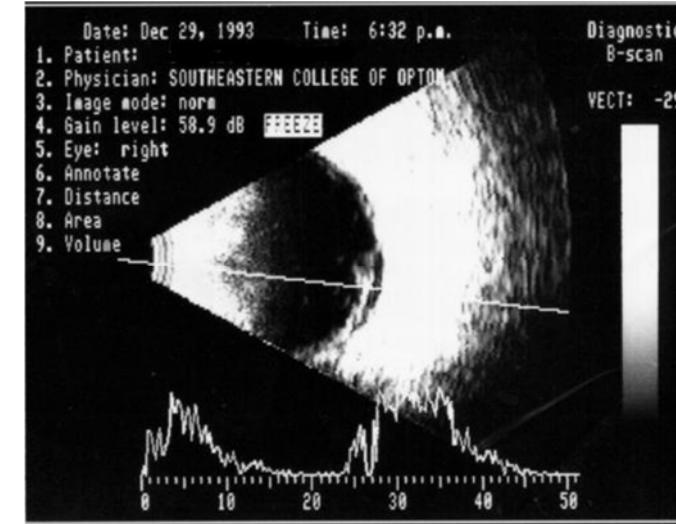
TM-mode



Textbook Fig. VIII.34

33

2-dimensional B-mode and A-mode (used in ophthalmology)



34

real speed of propagation for the accurate determination of distances:

cornea: 1641 m/s

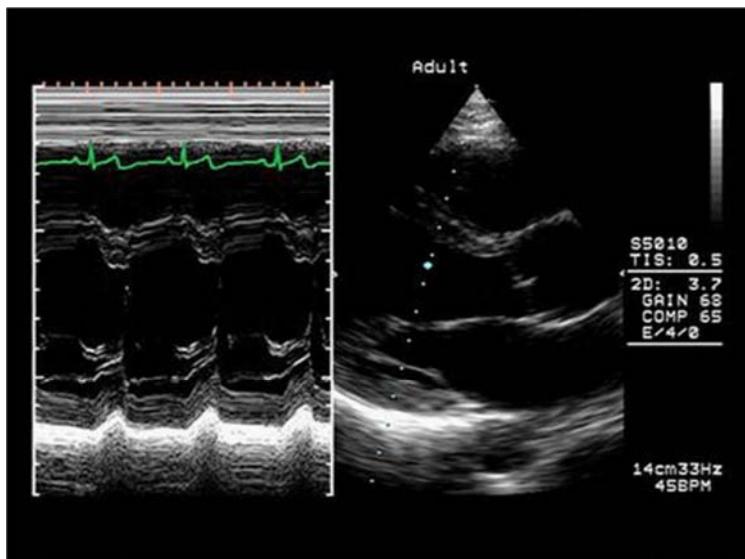
aqueous humour: 1532 m/s

crystalline lens: 1641 m/s

vitreous body: 1532 m/s

TM-mode

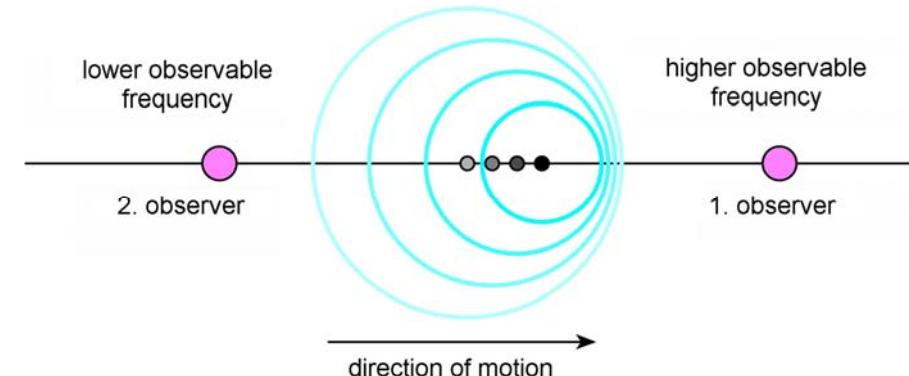
B-mode



35

Doppler phenomenon

„The pitch of a train whistle seems to get higher as it approaches, then seems to lower as the train whistle moves away.“ (C. Doppler, 1842)



Textbook Fig. VIII.39

36

f' : observed frequency, f : original frequency

- (a) standing source and moving observer (v_o)
+: observer approaches the source
-: observer moves away from the source

$$f' = f \left(1 \pm \frac{v_o}{c} \right)$$

- (b) moving source and standing observer
(if $v_s \ll c$, then „same” as (a))

$$f' = \frac{f}{1 \mp \frac{v_s}{c}}$$

- (c) moving source and moving observer

$$f' = f \frac{1 \pm \frac{v_o}{c}}{1 \mp \frac{v_s}{c}}$$

- (d) moving reflecting object (surface),
(if $v_r \ll c$)

$$f' = f \left(1 \pm \frac{2v_r}{c} \right)$$

37

Doppler frequency = frequency change = frequency shift

if $v_i, v_r \ll c$ ($i = S$ or O)

rearranging equation (a)

moving source or observer:

$$\Delta f = f_D = \pm \frac{v_i}{c} f$$

rearranging equation (d)

moving reflecting object or surface:

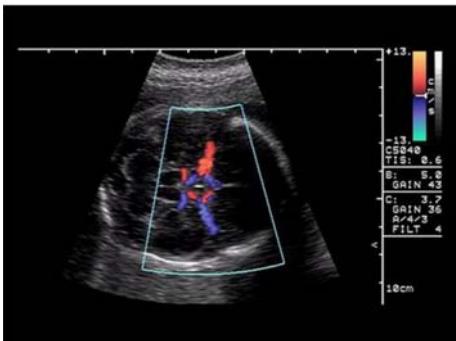
$$\Delta f = f_D = \pm 2 \frac{v_r}{c} f$$

if v and c are not parallel, then $v \cos \theta$ should be used instead of v (remark: if $\theta = 90^\circ$, $f_D = 0$)

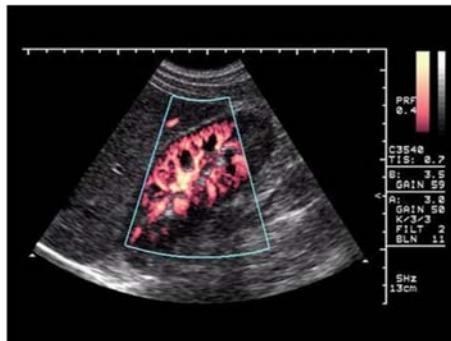
38

Colour coding

towards the transducer: warm colours
away from the transducer: cold colours



BART: Blue Away Red Towards



power Doppler

39

1-dimensional CW Doppler apparatus for measuring average flow velocity. Red blood cells as sound scatterers

CW: continuous wave

source and detector are separated

$$|f_D| = 2 \frac{v_r \cos \theta}{c} f$$

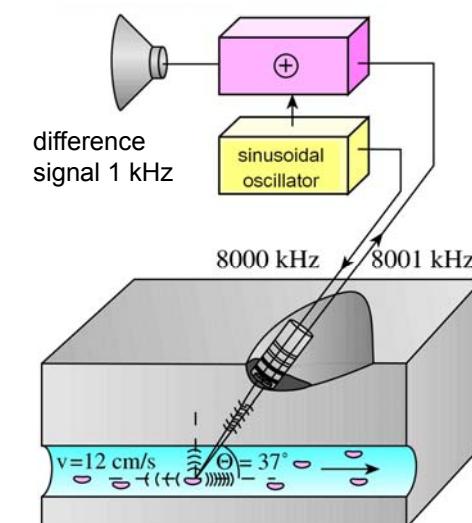
e.g. $f = 8000$ kHz

$v = 12$ cm/s

$c = 1600$ m/s

$\theta = 37^\circ$

$\Rightarrow f_D = 1$ kHz
(beating phenomenon)



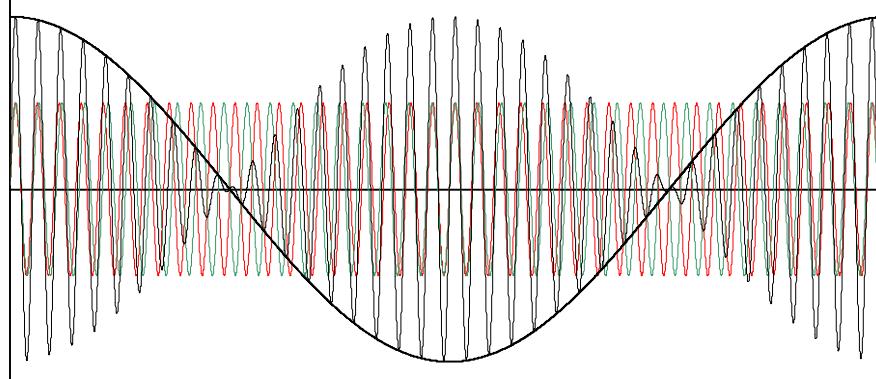
Textbook Fig. VIII.41

40

Beating phenomenon

$$f_{\text{red}} \geq f_{\text{green}}$$

the beating frequency equals to the difference of the two interfering frequency

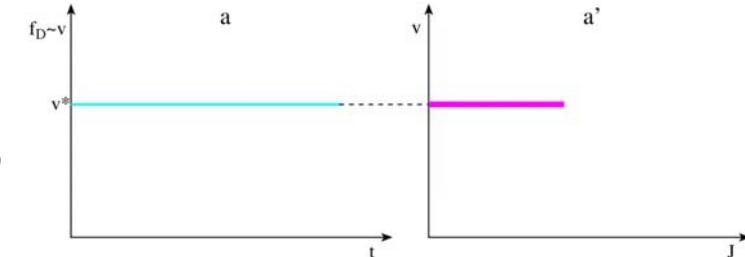


$$\text{reminder: } \sin \alpha + \sin \beta = 2 \sin \frac{\alpha + \beta}{2} \cos \frac{\alpha - \beta}{2}$$

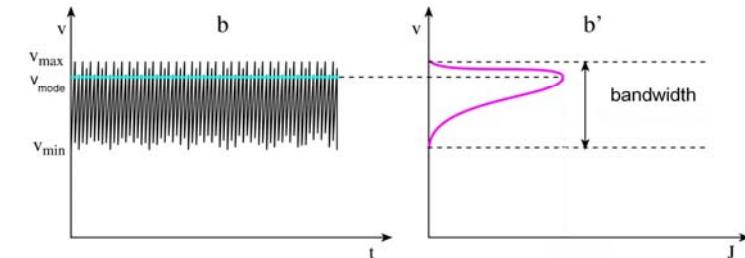
41

Doppler curves

one constant velocity (v^*)



frequency distribution (with v_{mode})



velocity distribution in TM-mode

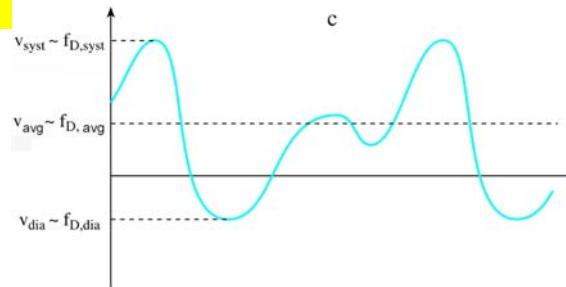
velocity distribution at a certain time

42

Textbook Fig. VIII.42

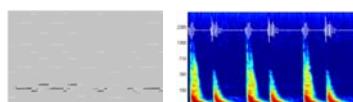
Doppler curves

flow can be represented by one velocity in each moment



Textbook Fig. VIII.42

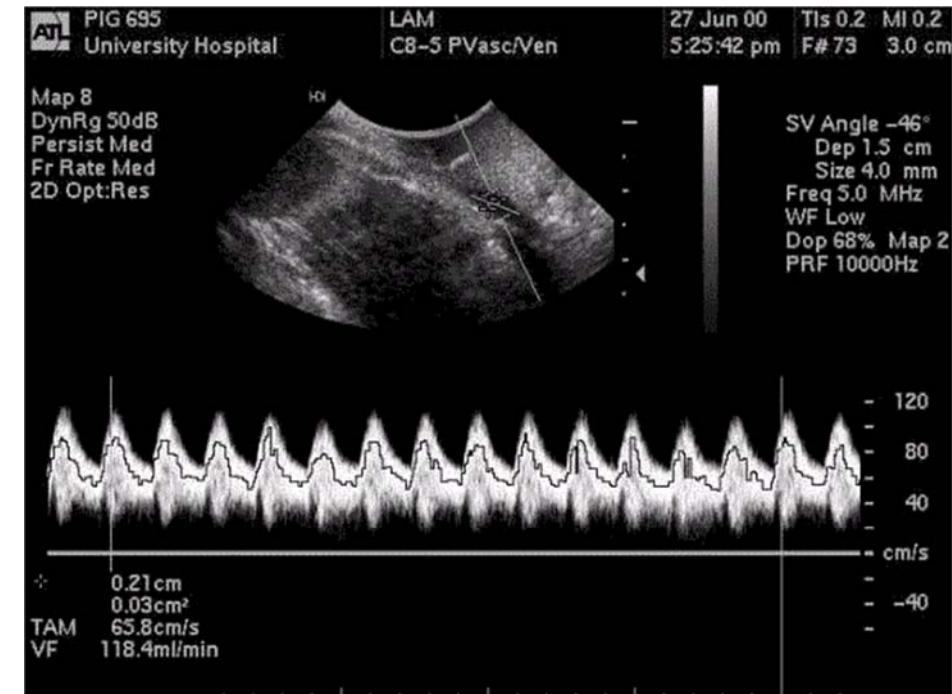
flow can be represented by a velocity distribution in each moment

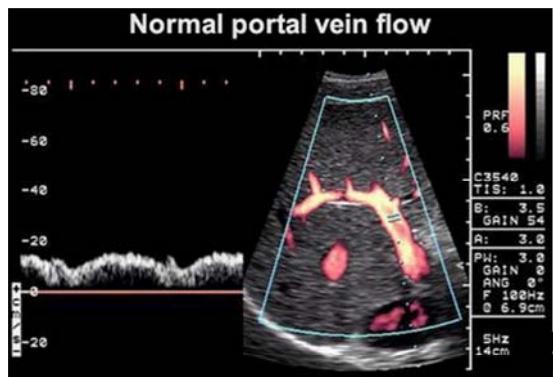


cf. voiceprint, music/heart beats in time-frequency representation

velocity distribution in TM-mode

43

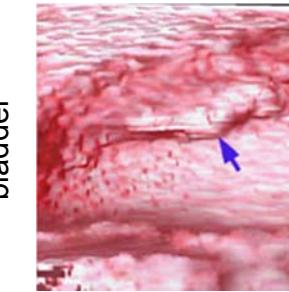




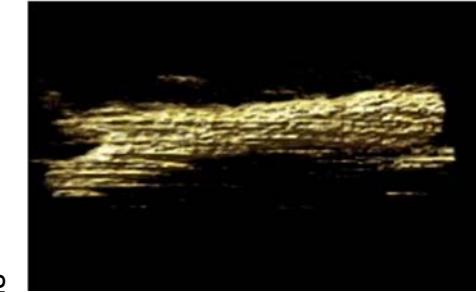
face of a fetus



bladder



3D reconstruction



Safety

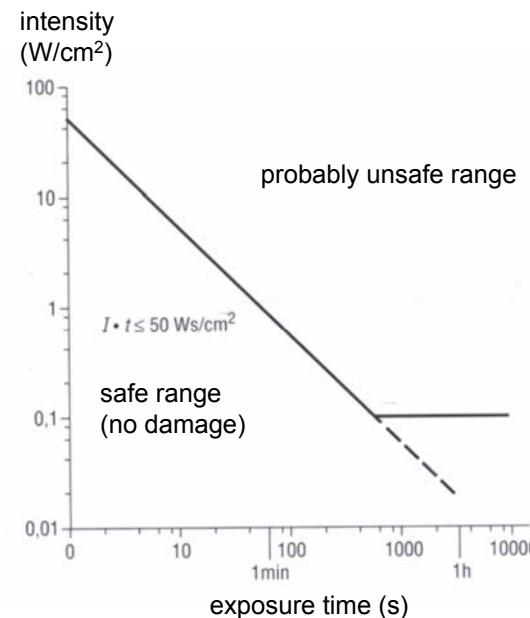
in the diagnostics:

$$10 \text{ mW/cm}^2 = 100 \text{ W/m}^2$$

cf. pain threshold: 10 W/m^2

in the therapy: 1 W/cm^2

spatial average temporal average (SATA) intensity;
spatial peak temporal peak (SPTP) intensity;
spatial peak temporal average (SPTA) intensity;
spatial peak pulse average (SPPA) intensity
spatial average pulse average (SAPA) intensity



more:

in „Medical imaging methods“
lecture + practice

